

# Fate of Ammonia in Refinery Amine Systems

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## INTRODUCTION

Ammonia ingress and accumulation in refinery and bio-gas amine systems is not a new problem. However, increasing utilization of advantaged crudes with higher nitrogen content may present challenges in today's capital-constrained operating environment. Many refiners have instituted guidelines for purging amine regenerator reflux water for corrosion control. Historically, this has been done empirically based upon periodic lab analysis and adjustment of the purge water rate.

The true amount of ammonia ingress, and its material balance across refinery amine unit is not a topic that has been discussed in great detail, because until now, rate-based mass transfer models have not been available. Using the well-known ProTreat™ rate-based mass transfer process simulator, this paper addresses the following questions. Where available, comparisons to plant data measurements are provided.

1. How much ammonia can accumulate based upon choice of regenerator operating conditions?
2. How much ammonia rejection into the amine acid gas does this correspond to, and is this a significant concern to downstream (i.e., sulfur plant) operations?
3. Can ammonia build to levels that will cause additional H<sub>2</sub>S to be trapped leading to higher lean loadings, reduced treating performance, or even regenerator flooding?
4. How much ammonia skates through refinery amine treaters?

Ultimately, we attempt to answer whether the ammonia balance on a refinery amine system can be fully characterized based upon the knowledge of a few simple parameters.



***ProTreat***<sup>TM</sup>

Taking the Guesswork Out of Gas Treating

**The Fate of Ammonia  
in Refinery Amine Systems**

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**Optimized Gas Treating, Inc.**

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# Objectives of Effort

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- Understand  $\text{NH}_3$  Ingress and Accumulation in Refinery Amine Systems
  - Quantify ingress and absorber pickup
  - How much can accumulate?
  - Impact of operating variables on accumulation
  - Accumulation effects on unit performance and reliability
  - Comparisons vs. real plant data



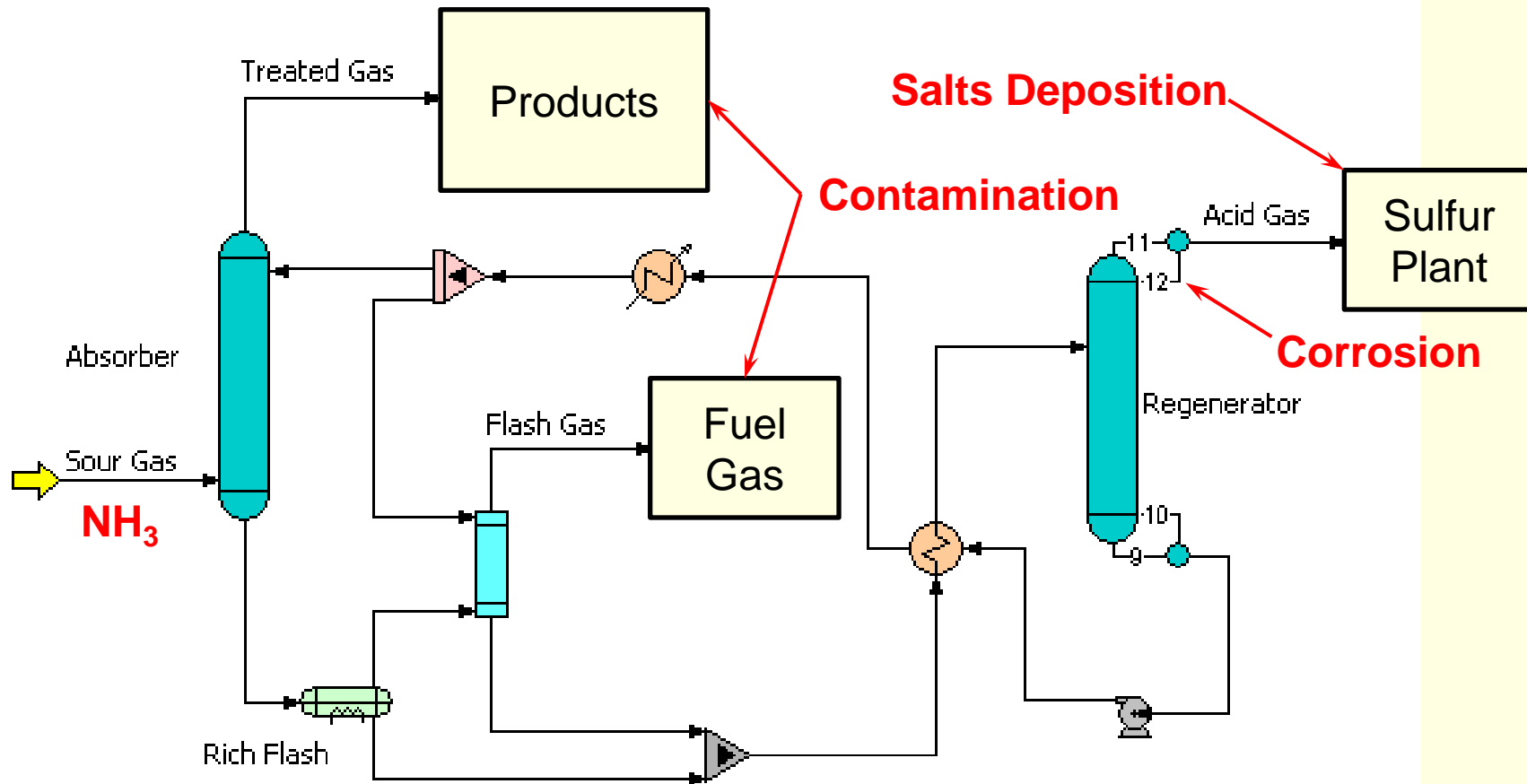
# Background & Relevance

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- $\text{NH}_3$  is an Amine
  - Simplest form possible
  - Volatile (lacks bulky alcohol chains)
  - Loves water
  - Reacts with and traps acid gases
- Acid Gases ( $\text{H}_2\text{S} + \text{CO}_2$ )
  - Toxic
  - Corrode steel in aqueous solution
  - Environmental concerns



# Ammonia Volatility Ramifications





# About the Model

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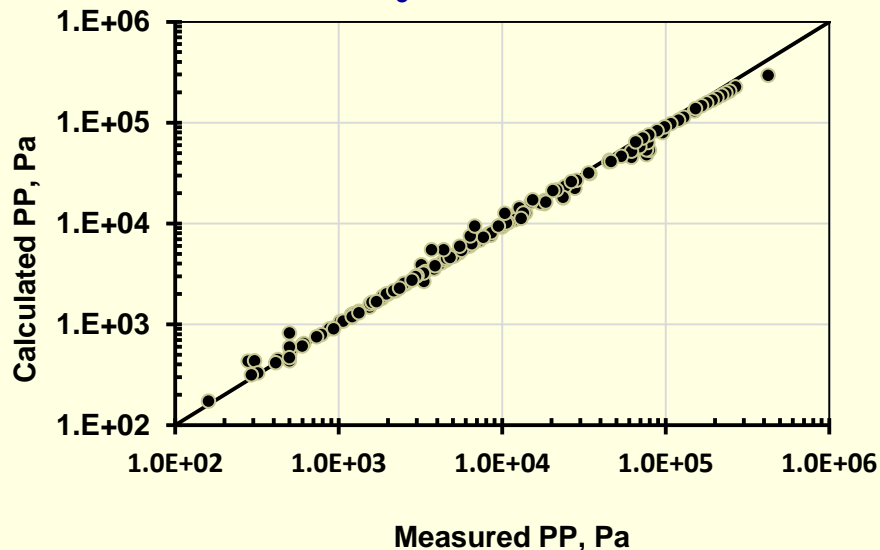
- Same basis as ProTreat™ for amines
- Mass transfer rate-based for  $\text{H}_2\text{S}$ ,  $\text{CO}_2$ ,  $\text{NH}_3$ ,  $\text{H}_2\text{O}$  transport; equilibrium for inerts; includes kinetics
- All separations equipment characterized by individual phase mass transfer coefficient and interfacial area correlations — similar to HTXR calculations
- Fully predictive — NO GUESSWORK, no efficiencies, no HETPs, no ideal stages, don't have to know the answer first!!! but...
- Can back efficiencies out if you want to see them
- Right answers out of the box without fitting — just data from P&IDs and internals vendor data sheets



# ProTreat™

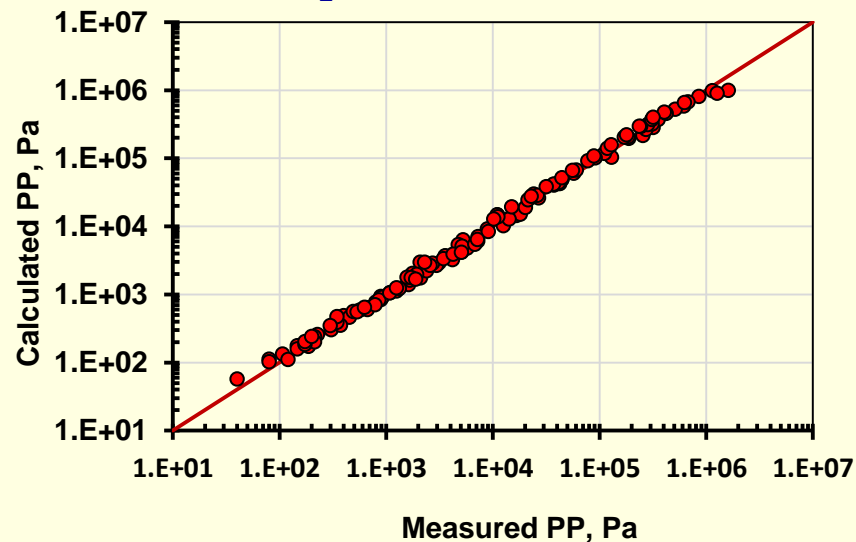
## How good is the VLE model?

### NH<sub>3</sub> Partial Pressure



Data Sources: API 955, GPA RR-118 and Maurer (1999)

### H<sub>2</sub>S Partial Pressure

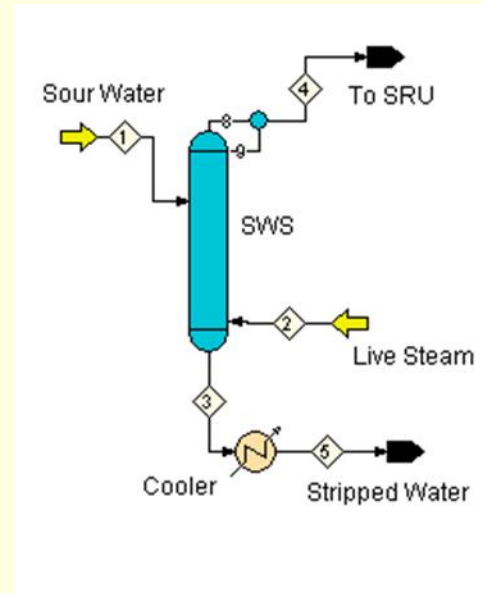
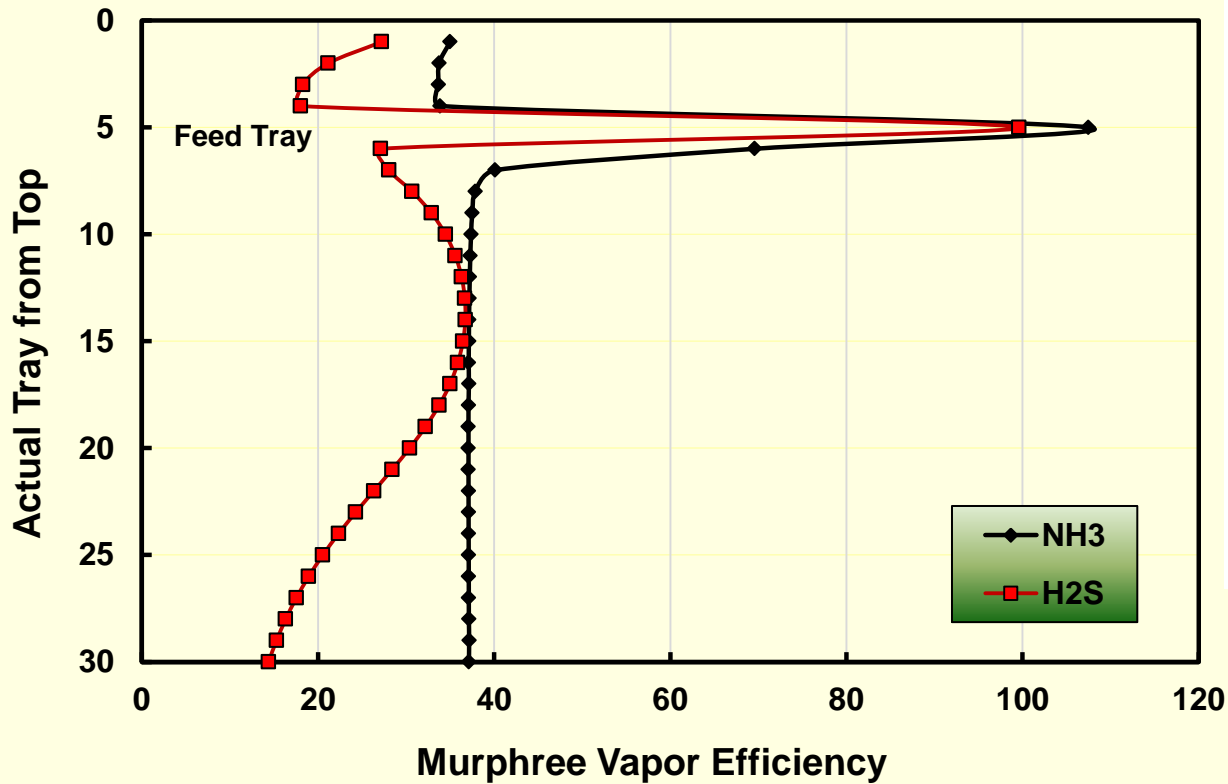


Partial Pressure (Calc/Meas)	Avg.	Std. Dev.
NH <sub>3</sub>	1.004	0.149
H <sub>2</sub> S	1.030	0.149
CO <sub>2</sub>	1.043	0.185



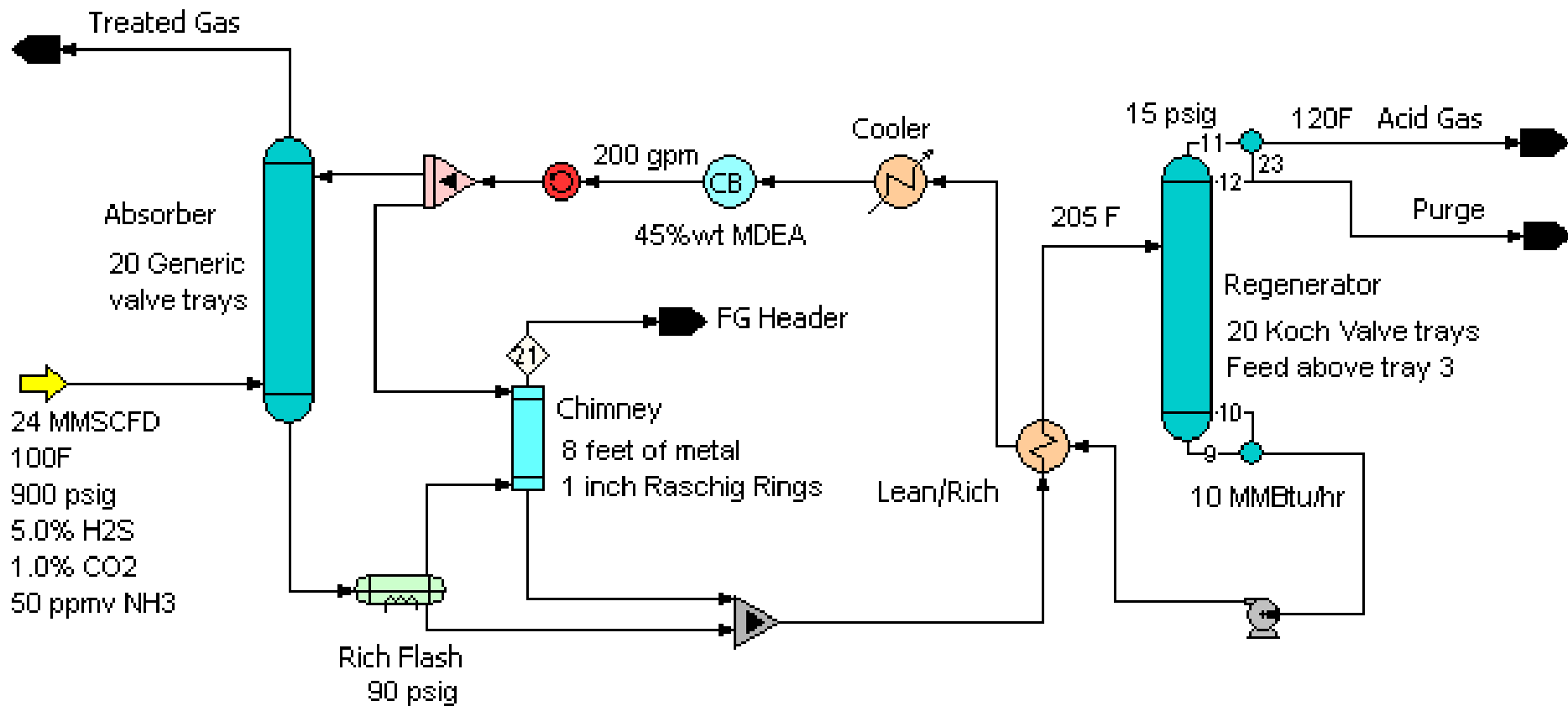
# ProTreat™

## Efficiencies for $H_2S$ and $NH_3$ Stripping





# Basis for Parametric Studies





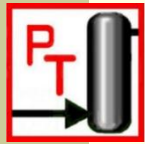
# Parametric Study

- Absorber Pickup
  - Sour gas temperature: 100°F, 120°F, 140°F
  - Lean amine temperature: Sour gas + 10F  $\Delta T$
  - Feed Pressure: 900 psig, 450 psig, 125 psig
  - NH<sub>3</sub> in Feed: 50, 150, 500 ppmv (dry)
- Accumulation Studies
  - Condenser temperature: 120°F, 140°F, 160°F
  - Purge reflux water



# Absorber NH<sub>3</sub> Pickup

Parameter	Base Case	Elevated Temperature		Lower Absorber Pressure	
Inlet Gas Temperature °F	100	120	140	100	100
Lean Amine Temp, °F	110	130	150	110	110
Absorber Pressure, psig	900	900	900	450	125
NH <sub>3</sub> Conc. In Feed, ppmv	50	50	50	50	50
% NH <sub>3</sub> pickup in Absorber	97.5	96.9	96.2	96.5	91.5
ppmv NH <sub>3</sub> in Treated Gas	1.3	1.6	2.0	1.9	4.4
wt % NH <sub>3</sub> in reflux water	1.35	1.35	1.36	1.37	1.35
Lean H <sub>2</sub> S loading	0.0084	0.0082	0.0080	0.0083	0.0081
Lean CO <sub>2</sub> loading	0.0003	0.0003	0.0003	0.0003	0.0003
Treated Gas, ppmv H <sub>2</sub> S	7.9	11.6	17.7	12.8	96
ppmw NH <sub>3</sub> in lean amine	16.2	13.7	11.9	14.5	10.1
% CO <sub>2</sub> pickup in Absorber	80.5	75.3	68.7	63.1	21.1
NH <sub>3</sub> in Acid Gas, %vol (wet)	0.072	0.072	0.074	0.074	0.073



# Effect of NH<sub>3</sub> Concentration

Parameter	Base Case	Higher NH <sub>3</sub> Feed Content	
Inlet Gas Temperature °F	100	100	100
Lean Amine Temp, °F	110	110	110
Absorber Pressure, psig	900	900	900
NH <sub>3</sub> Conc. In Feed, ppmv	50	150	500
% NH <sub>3</sub> pickup in Absorber	97.5	98.3	98.7
ppmv NH <sub>3</sub> in Treated Gas	1.3	2.8	7.0
wt % NH <sub>3</sub> in reflux water	1.35	2.60	5.21
Lean H <sub>2</sub> S loading	0.0084	0.0085	0.0086
Lean CO <sub>2</sub> loading	0.0003	0.0003	0.0004
Treated Gas, ppmv H <sub>2</sub> S	7.9	8.0	8.2
ppmw NH <sub>3</sub> in lean amine	16.2	33.8	85.4
% CO <sub>2</sub> pickup in Absorber	80.5	80.6	80.8
NH <sub>3</sub> in Acid Gas, %vol (wet)	0.072	0.23	0.77



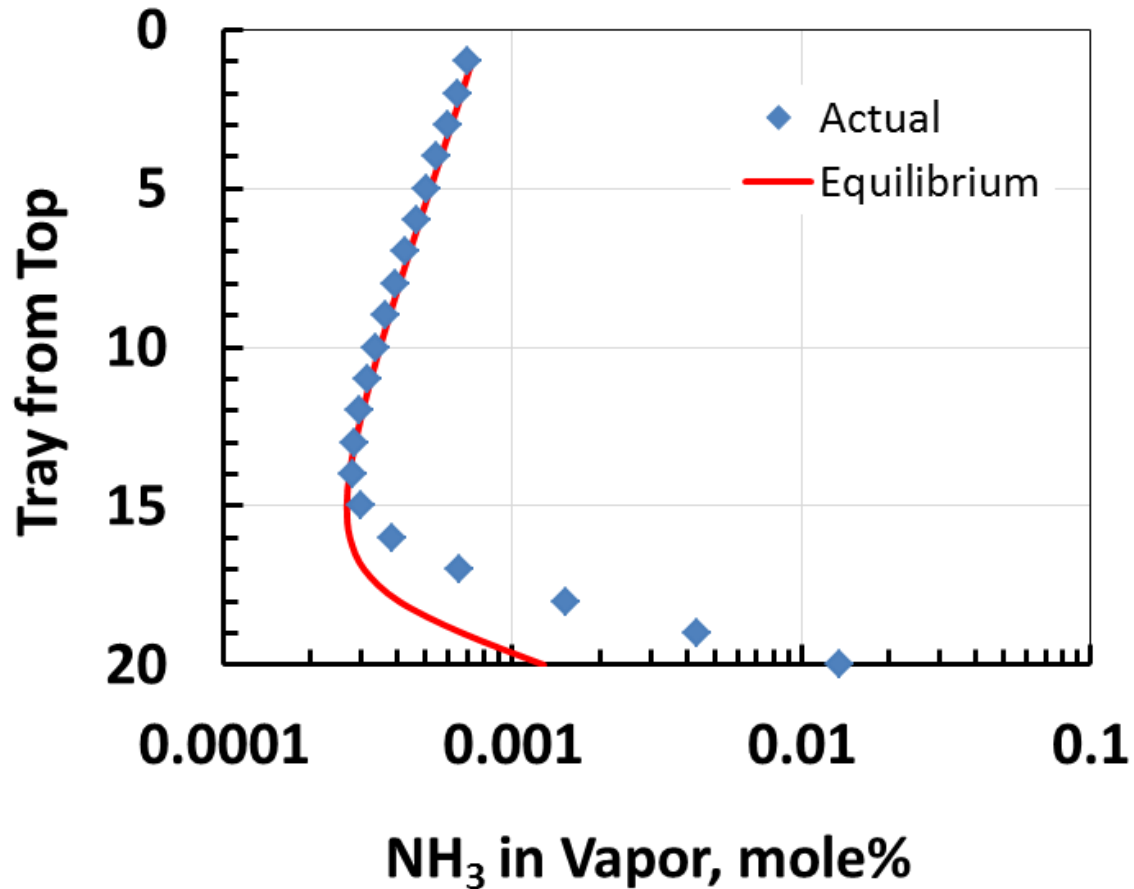
# Absorber Pickup Conclusions

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- Higher temperature and lower pressure reduce  $\text{NH}_3$  pickup
- $\text{NH}_3$  pickup efficiency increases with partial pressure in the feed
- $\text{NH}_3$  slip into treated gas is controlled by residual  $\text{NH}_3$  levels in the lean amine
- $\text{CO}_2$  pickup is only marginally increased so the presence of  $\text{NH}_3$  does not significantly “activate” the MDEA at these low levels.

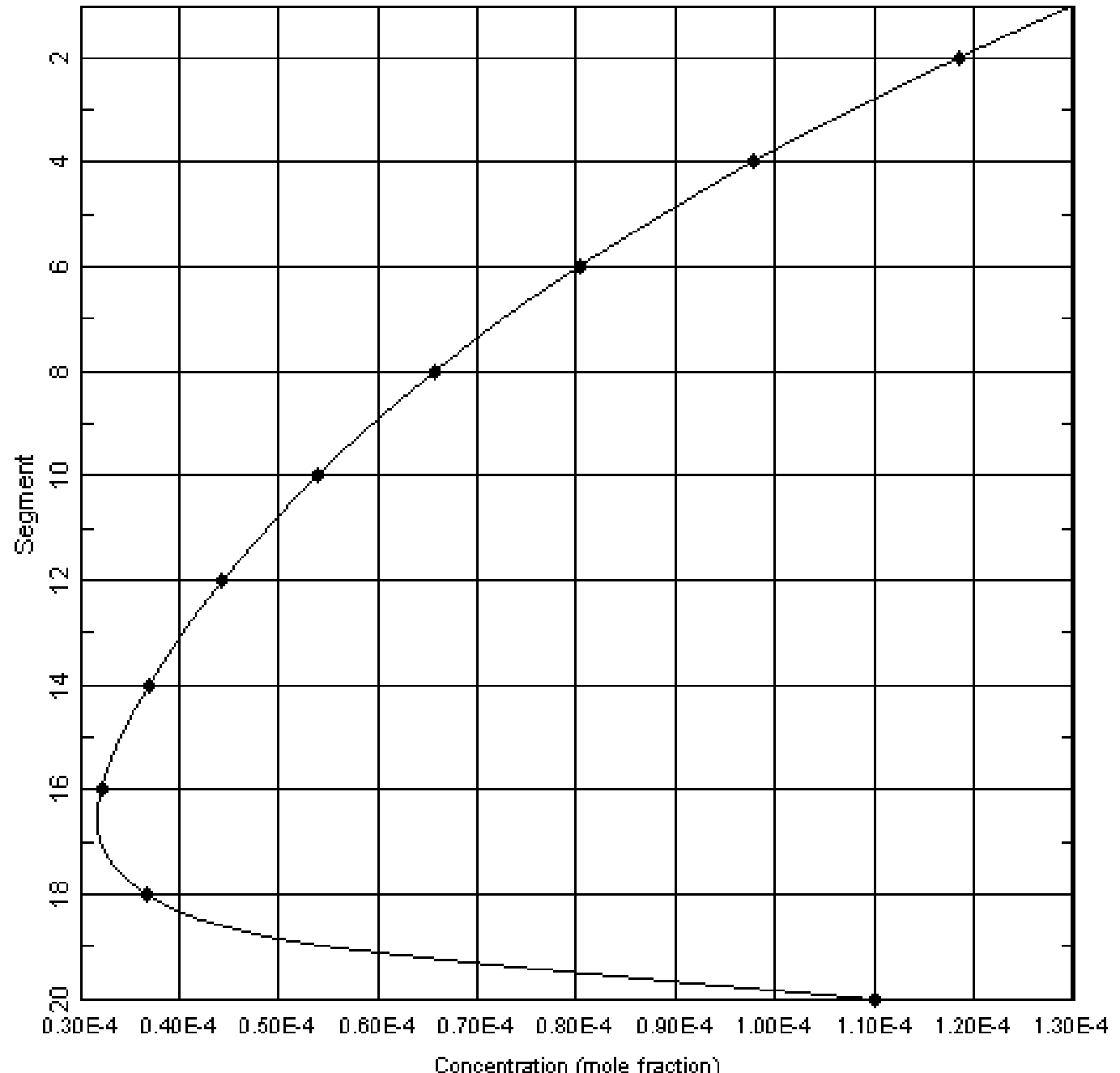


# NH<sub>3</sub> Vapor Profile in Absorber



- Above tray 15, NH<sub>3</sub> is stripped from the solvent by “lean gas”
- Below tray 15, H<sub>2</sub>S and CO<sub>2</sub> pickup are significant, which binds NH<sub>3</sub> into solution as NH<sub>4</sub><sup>+</sup> and NH<sub>3</sub>COO<sup>-</sup>

Absorber: NH3 Ionic Concentration





# Accumulation vs. Condenser Temperature

NH <sub>3</sub> Conc. In Feed, ppmv	150	150	150	500	500	500
Condenser Temperature °F	120	140	160	120	140	160
% NH <sub>3</sub> pickup in Absorber	98.3	99.0	99.4	98.7	99.2	99.5
ppmv NH <sub>3</sub> in Treated Gas	2.8	1.7	1.0	7.0	4.3	2.9
wt % NH <sub>3</sub> in reflux water	2.60	1.42	0.76	5.21	2.90	1.59
Lean H <sub>2</sub> S loading	0.0085	0.0084	0.0083	0.0086	0.0085	0.0084
Lean CO <sub>2</sub> loading	0.0003	0.0003	0.0003	0.0004	0.0003	0.0003
Treated Gas, ppmv H <sub>2</sub> S	8.0	7.8	7.7	8.2	8.0	7.8
ppmw NH <sub>3</sub> in lean amine	33.8	20.3	12.6	85.4	52.5	35.4
% CO <sub>2</sub> pickup in Absorber	80.6	80.6	80.5	80.8	80.7	80.7
NH <sub>3</sub> in Acid Gas, %vol (wet)	0.23	0.22	0.21	0.77	0.75	0.70





# Condenser Temperature Conclusions

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- Effective at driving  $\text{NH}_3$  into the acid gas.
  - Helps to remove more  $\text{NH}_3$  in the absorber
  - $\text{H}_2\text{S}$  treat marginally improved due to lower lean loading (less reflux and  $\text{NH}_3$  + trapped  $\text{H}_2\text{S}$  to restrip)
  - Reflux circuit corrosion may not be reduced due to the higher temperature offset
- Bad for the sulfur plant



# Effect of Reflux Purging

NH <sub>3</sub> Conc. In Feed, ppmv	500	500	500	500
% Reflux Water Purged	0	15	75	51*
% NH <sub>3</sub> pickup in Absorber	98.7	99.1	99.7	99.3
ppmv NH <sub>3</sub> in Treated Gas	7.0	4.7	1.8	3.5
wt % NH <sub>3</sub> in reflux water	5.21	3.87	1.6	0.99
Lean H <sub>2</sub> S loading	0.0086	0.0085	0.0081	0.0086
Lean CO <sub>2</sub> loading	0.0004	0.0003	0.0003	0.0003
Treated Gas, ppmv H <sub>2</sub> S	8.2	8.0	7.4	8.1
ppmw NH <sub>3</sub> in lean amine	85.4	57.4	21.7	42.9
% CO <sub>2</sub> pickup in Absorber	80.8	80.8	80.7	80.7
NH <sub>3</sub> in Acid Gas, %vol (wet)	0.77	0.46	0.10	0.17



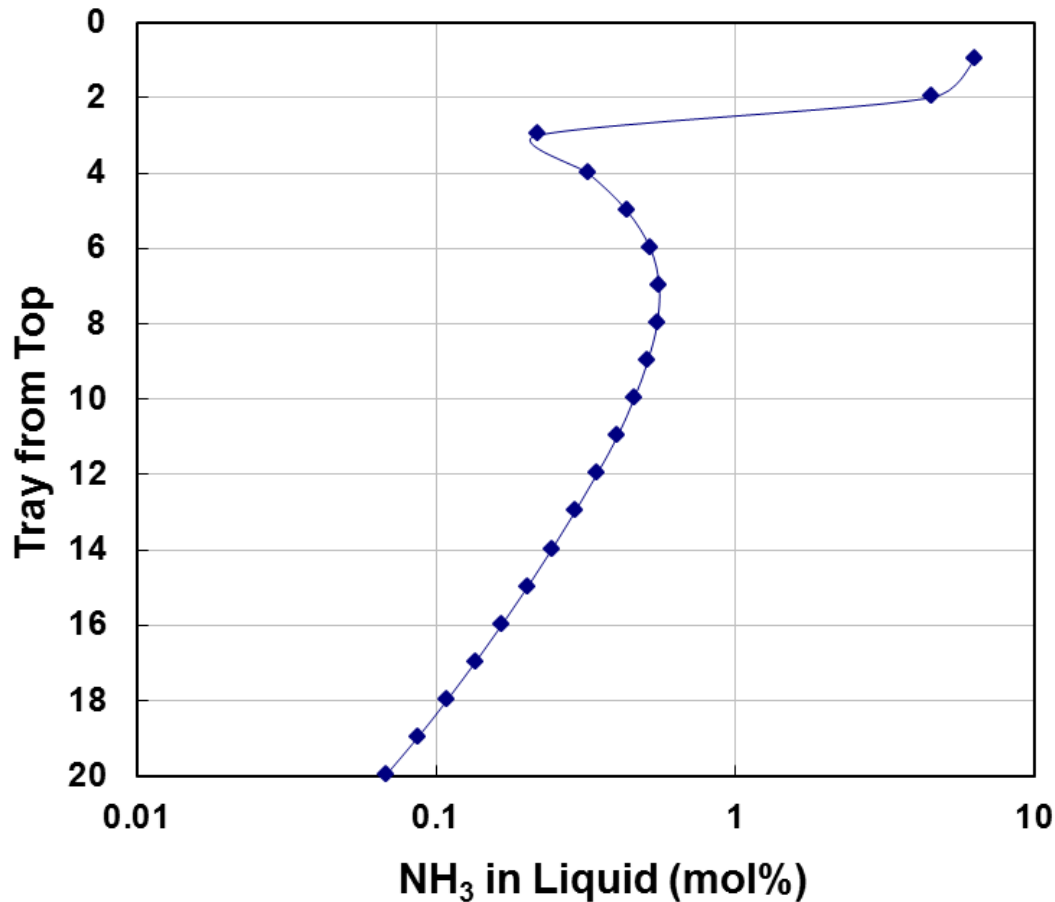
# Reflux Purging Conclusions

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- Effective at removing  $\text{NH}_3$  from the amine system
- Minimizes  $\text{NH}_3$  slip into acid gas
- Reduces corrosion in the reflux system
- Fresh water make-up into the reflux amplifies benefits



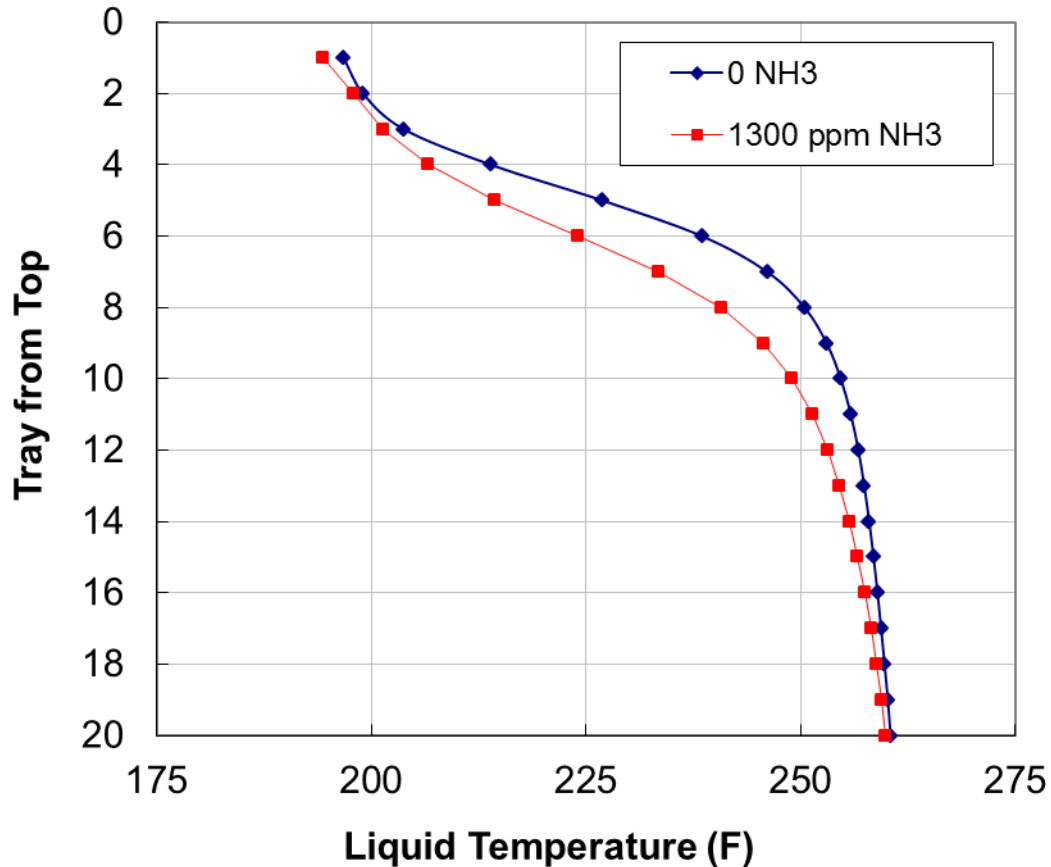
# Regenerator Profile (Unpurged)



- NH<sub>3</sub> accumulation is not constrained to the reflux wash section.
- Accumulates well below the feed tray
- Incremental heat of reaction → higher reboiler duty or....



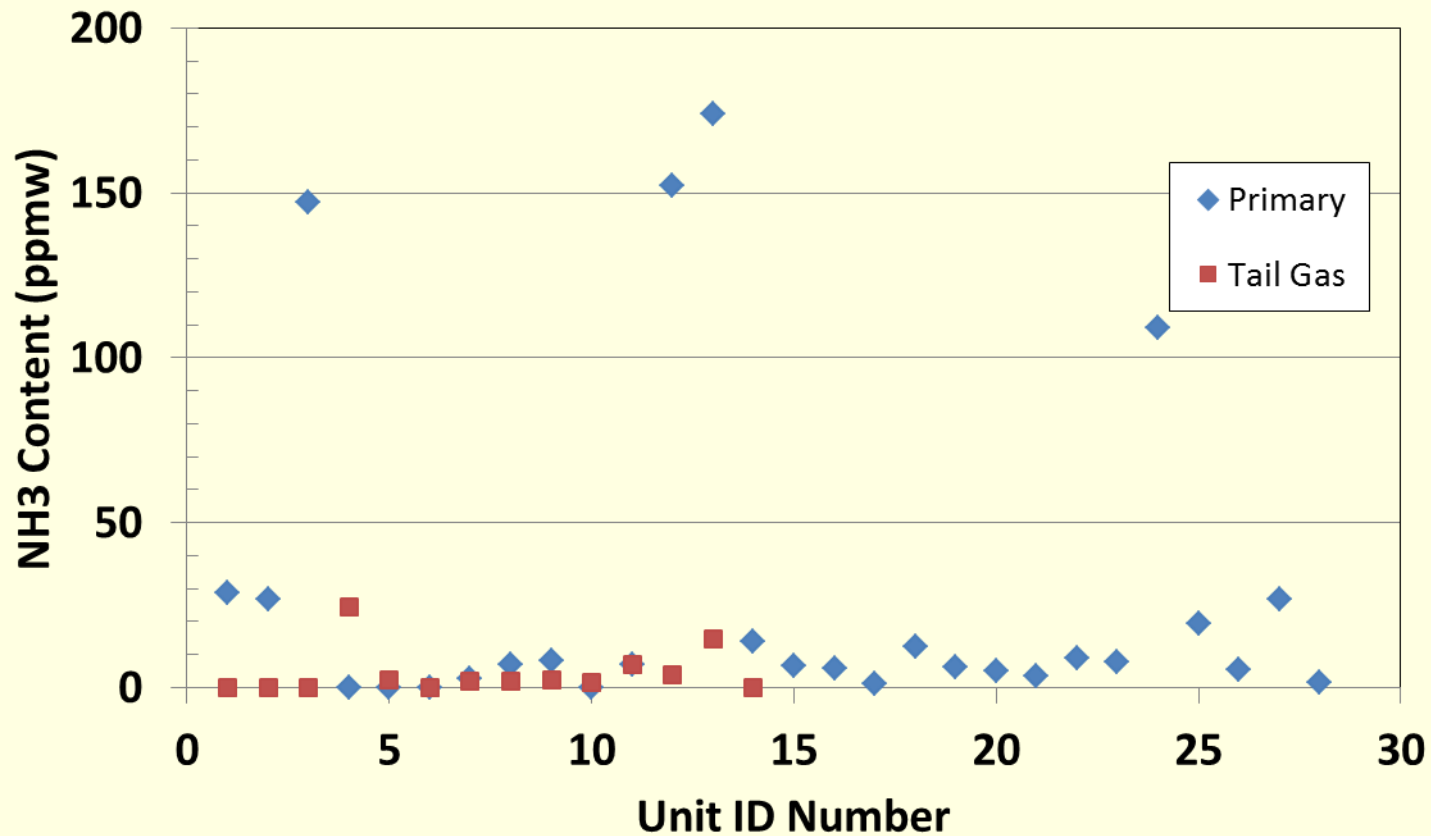
# Slumped Regeneration Temperatures With $\text{NH}_3$



- At constant reboiler duty, more energy goes into boiling and condensing  $\text{NH}_3$  and trapped  $\text{H}_2\text{S}$
- “Foaming” is an urban legend as vapor traffic is reduced.

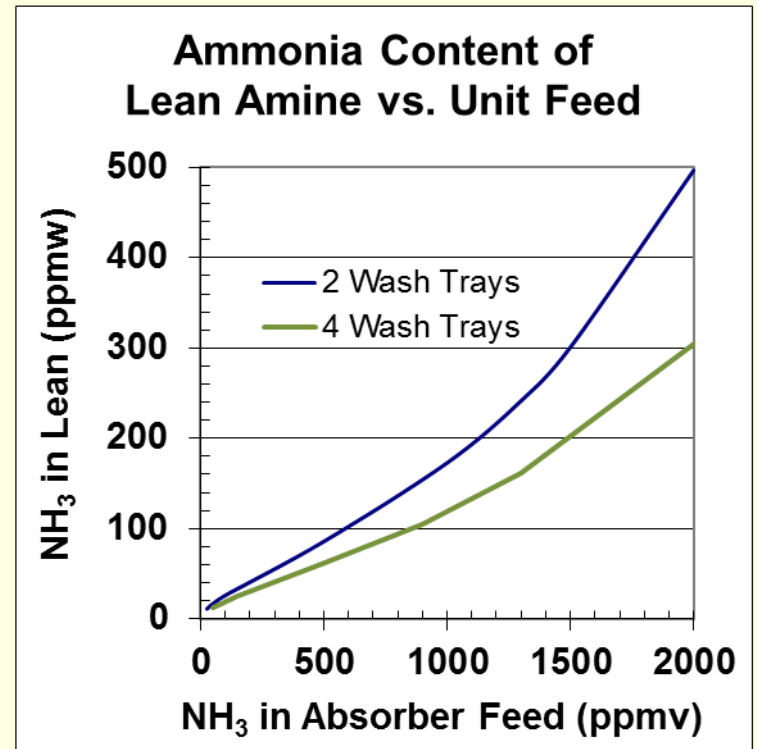
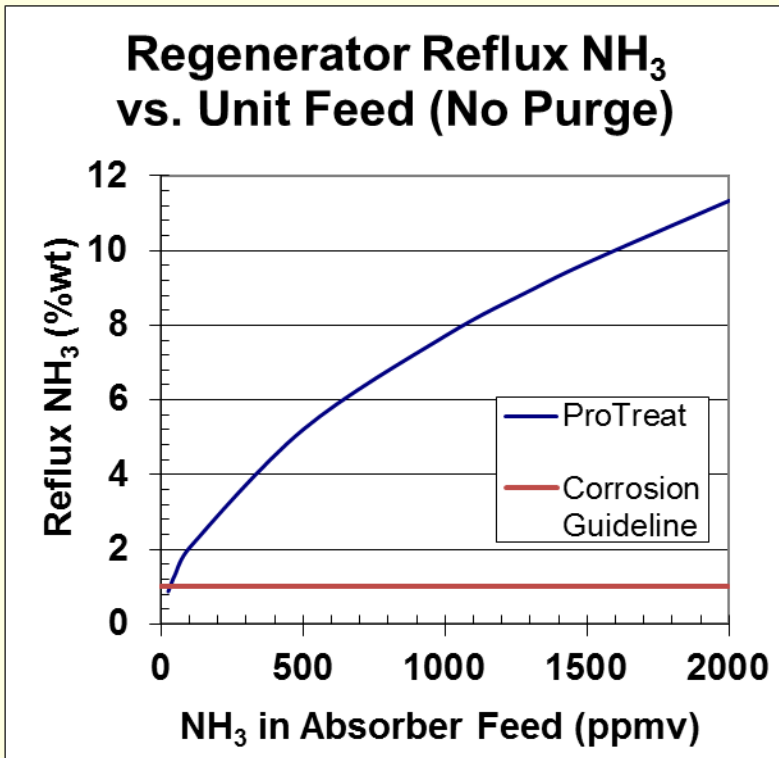


# Measured $\text{NH}_3$ in Lean Amines



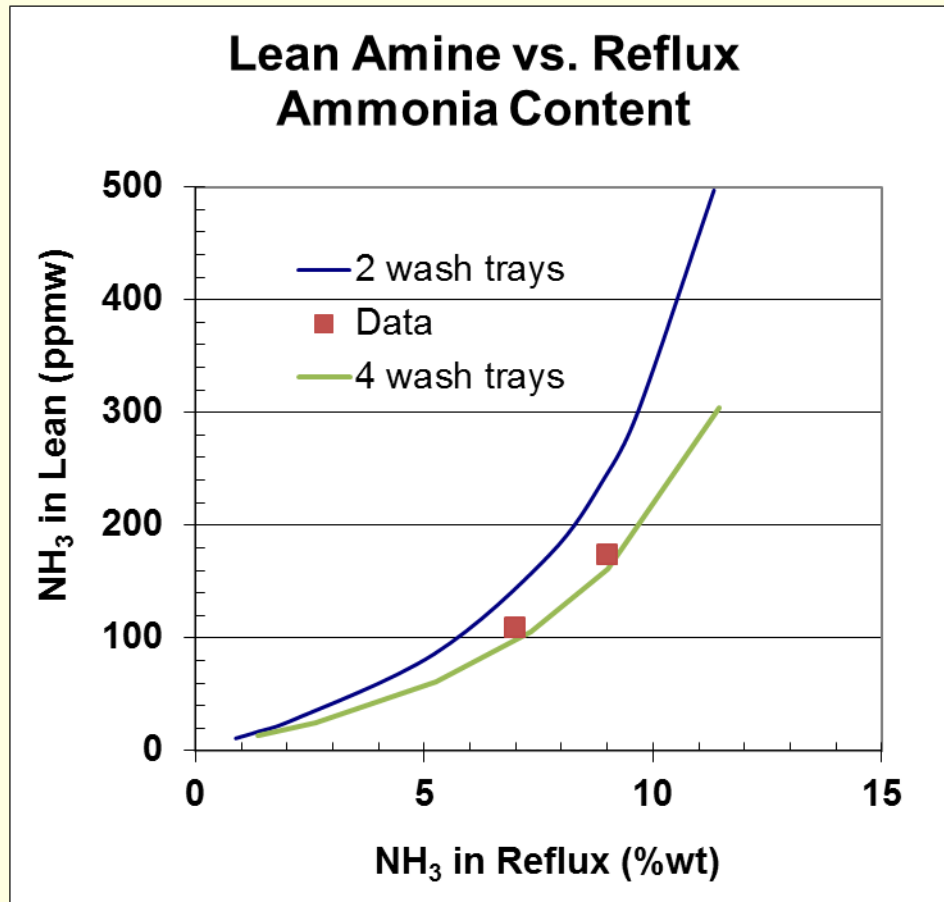


# NH<sub>3</sub> Levels in Unpurged Amine Units





# Plant Data Validation







## Conclusions

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- Very little  $\text{NH}_3$  contamination can lead to Regenerator reflux corrosion concerns and purging needs
- Ammonia slip to product streams can be expected and minimized by purging reflux
- Model provides some guidance on relationships between  $\text{NH}_3$  levels in unit feed, reflux, and acid gas
- Results depend upon unit configuration and should be viewed on a case-by-case basis



# Acknowledgments

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- Simon Weiland
- Scott Alvis & David Edward
- Al Keller